



University of Bradford
Department of Mechanical and
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CAMSHAFT TIMING-BELT RELIABILITY MODELLING

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AGENDA

- Aims & objectives
- Philosophy of the approach
- Camshaft timing-belt life modelling
- Use of the timing-belt life model & sensitivity analysis
- Discussion & conclusions

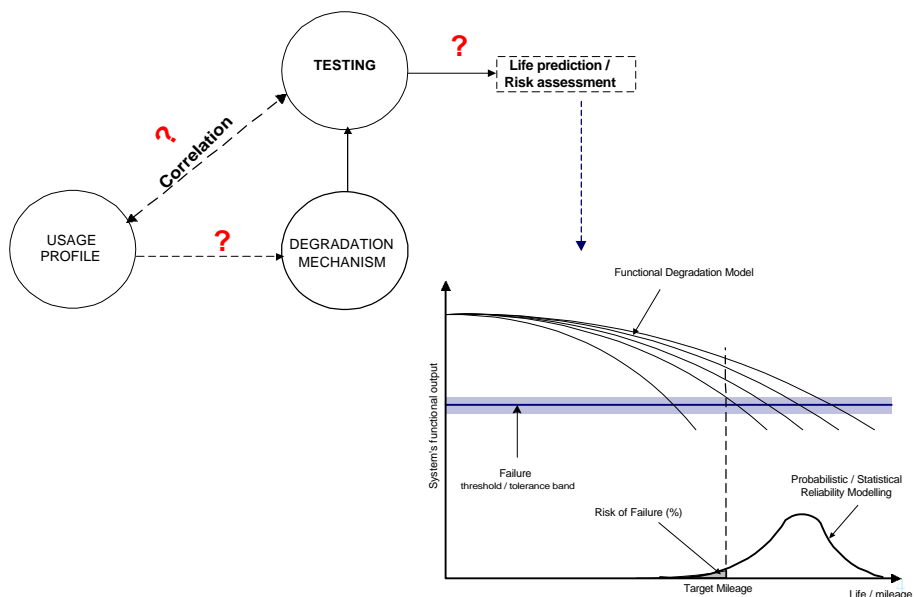
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Aims & Objectives of the Presentation

- To present a methodology for customer correlated life prediction modelling of automotive systems.
- To illustrate the practical application of this methodology with the camshaft timing-belt life model development -
model construction - calibration - validation
- To discuss the results obtained and to indicate direction for future development.

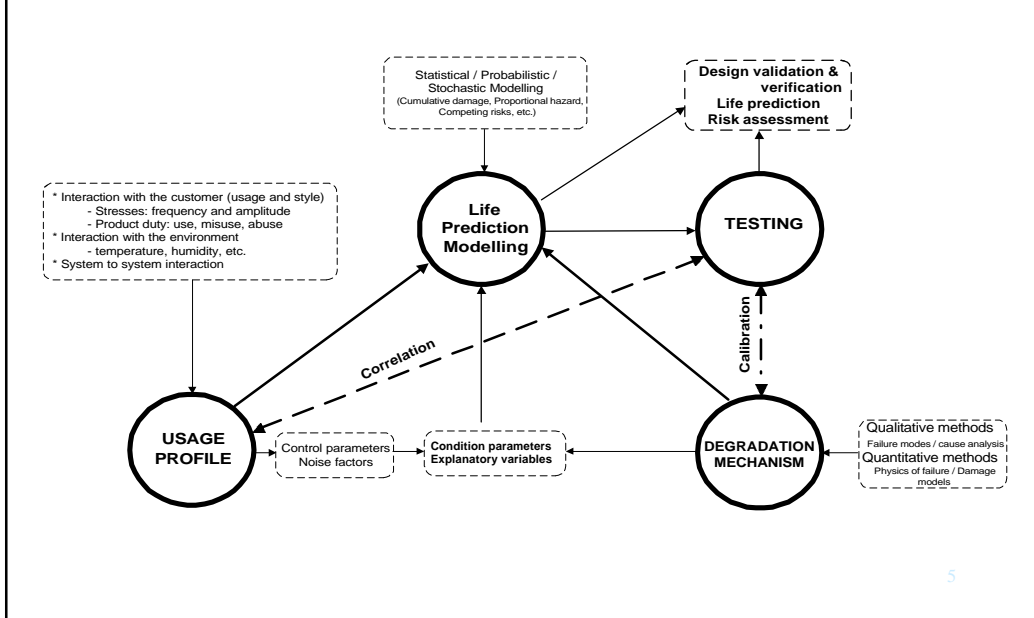
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Philosophy of the approach (1)



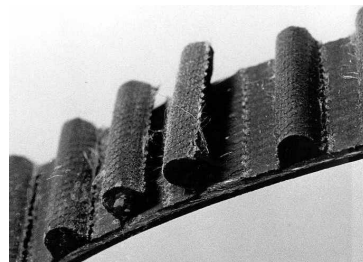
Philosophy of the approach (2)

Customer Correlated Life Prediction Modelling



Timing-belt Failure Mechanism

TRC (Tooth Root Cracking) -
shear fatigue failure mechanism.



Factors influencing the fatigue life of the timing belt:

- Mechanical properties of belt material - tooth stiffness.
- Design layout - belt/pulley number of teeth, tensioners, angle of wrap, belt width.
- *Tooth load - radial & tangential*
- *Tooth deflection*
- Operating temperature, ageing at temperature

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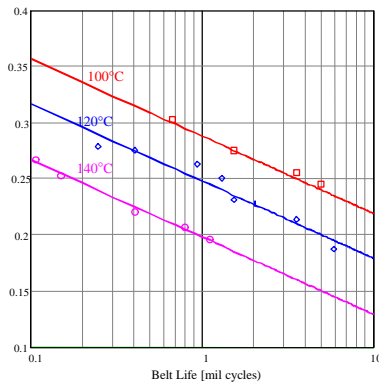
Timing Belt Fatigue Life Model

Dynamometer studies and modelling of the load sharing between teeth in fully meshed conditions showed a linear relationship between tooth deflection and log life.

$$\lambda = A - B \cdot \ln(N)$$

$$N(\lambda) = e^{-\frac{\lambda-A}{B}}$$

Proportional hazard modelling for the effect of operating temperature



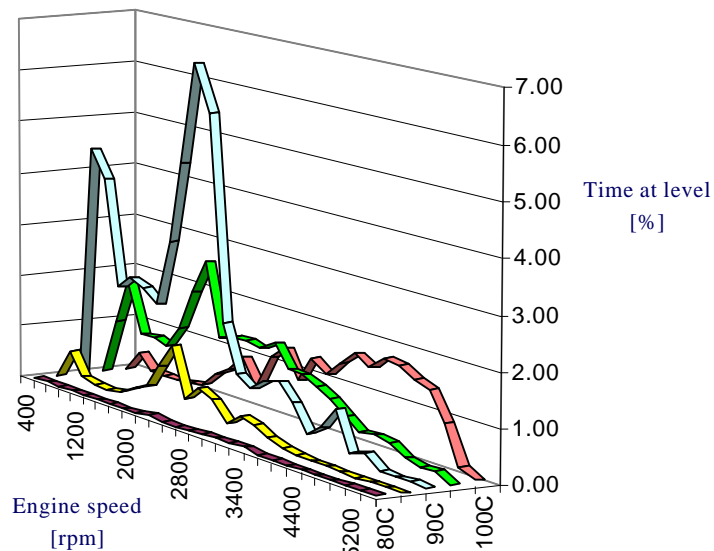
Arrhenius model was used for the influence of the belt operating temperature

Fatigue life of the timing belt:

$$N(\lambda; T) = C \cdot e^{\frac{D}{T}} \cdot e^{-\frac{\lambda-A}{B}}$$

$$N(\lambda; T) = 3.174 \cdot 10^{-13} \cdot e^{\frac{1.188 \cdot 10^4}{T}} \cdot e^{-\frac{\lambda-0.2}{0.029}}$$

Customer Usage Profile



Timing-belt Life Modelling

- Number of load cycles during a time unit (1 hour)

$$P_{ni} = \frac{M_c \cdot 60 \cdot \omega_i}{M_b}$$

- Damage accumulated at a certain level - engine speed / operating temperature

$$d_{i,j} = \frac{\alpha_{i,j} \cdot P_{ni}}{N(\lambda, T_j)}$$

- Damage accumulated during a time unit

$$D_m = \sum_i \sum_j d_{i,j} = \frac{M_c}{M_b} \cdot \frac{60}{C \cdot e^{\frac{\lambda-A}{B}}} \cdot \sum_i \omega_i \cdot \sum_j \alpha_{i,j} \cdot e^{-\frac{D}{T_j}}$$

- Timing-belt life model

$$L = \frac{C_m}{D_m} = C_m \cdot C \cdot e^{\frac{\lambda-A}{B}} \cdot \frac{M_b}{60 \cdot M_c} \cdot \frac{1}{\sum_i \omega_i \cdot \sum_j \alpha_{i,j} \cdot e^{-\frac{D}{T_{ji}}}}$$

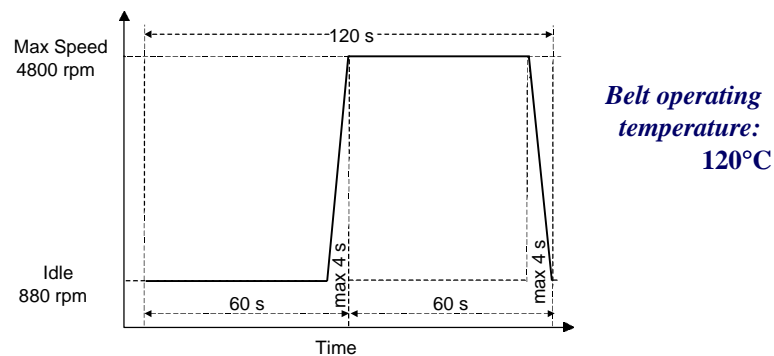
C_m - cumulated damage at failure (Miner's constant)

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Calibration of the Model

Objective: To assess the distribution of the cumulated damage at failure

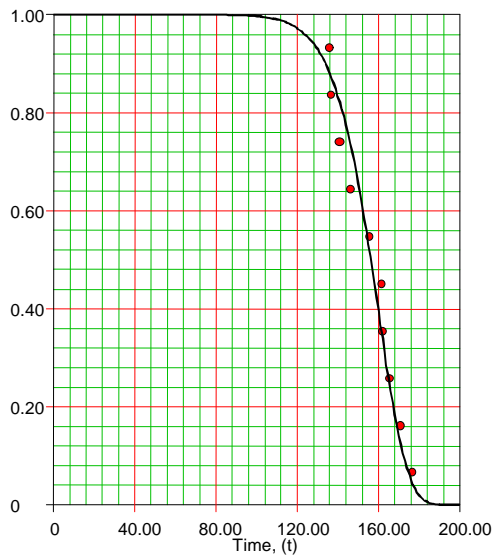
Engine Dynamometer Test Load Cycle:



Belt No.	1	2	3	4	5	6	7	8	9	10
Hours to failure	795	800	825	856	910	946	950	970	1000	1035
Tooth cycles to failure [$\times 10^6$]	135.5	136.3	140.6	145.9	155.1	161.2	161.9	165.3	170.4	176.4

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Weibull analysis of the test data



Percentiles of the distribution of cumulated damage at failure:

Median

$$C_{m50\%} = N_{50\%} \cdot D_m = 7.297$$

5th percentile

$$C_{m5\%} = N_{5\%} \cdot D_m = 5.671$$

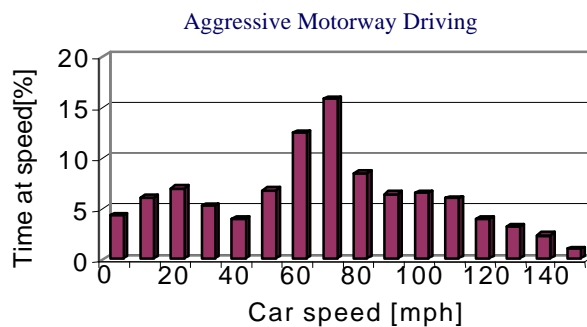
1st percentile

$$C_{m1\%} = N_{1\%} \cdot D_m = 5.281$$

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Use of the Timing-belt Life Model -

Life predictions under customer usage conditions

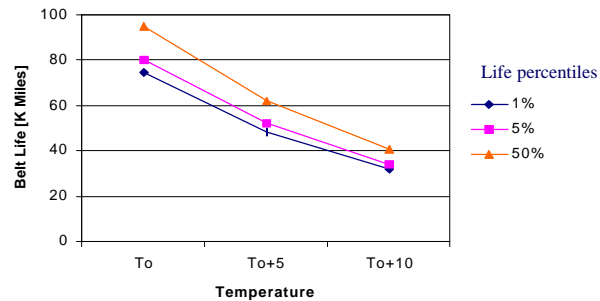


- **1st percentile** $Lf_{1\%} = 74,570$ miles
- **5th percentile** $Lf_{5\%} = 80,078$ miles
- **Median life** $Lf_{50\%} = 95,207$ miles

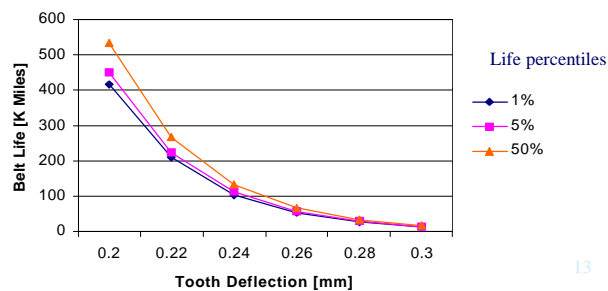
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Sensitivity Analysis on the Life Predictions

Influence of belt operating temperature



Influence of tooth deflection (Cam-belt system design)



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Discussion & Conclusions (1)

- Timing-belt life model can be used for life prediction or as a risk assessment tool, to validate the service intervals.
- Any engine dynamometer test can be used to calibrate the life model, i.e. there is no need to design a specific validation test for the timing belt!
The only requirement is that tests should be carried out to failure.
- To achieve reliability improvement, actions can be taken on:
 - cam-belt system design, to reduce the tooth deflection.
 - belt operating temperature.
- Life model can be used to validate the reliability improvement.

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Discussion & Conclusions (2)

- Development of the timing-belt life model illustrates the practical application of the “Customer Correlated Life Prediction Methodology”.
- Life modelling enables a better understanding of the stochastic nature of parameters and noises that define customer usage and their impact on the life of the automotive system.
- Customer correlated life prediction modelling gives a definite prospective for condition-based automotive servicing. The optimum moment for service can be determined by using stochastic damage accumulation and customer usage information from data logging.

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